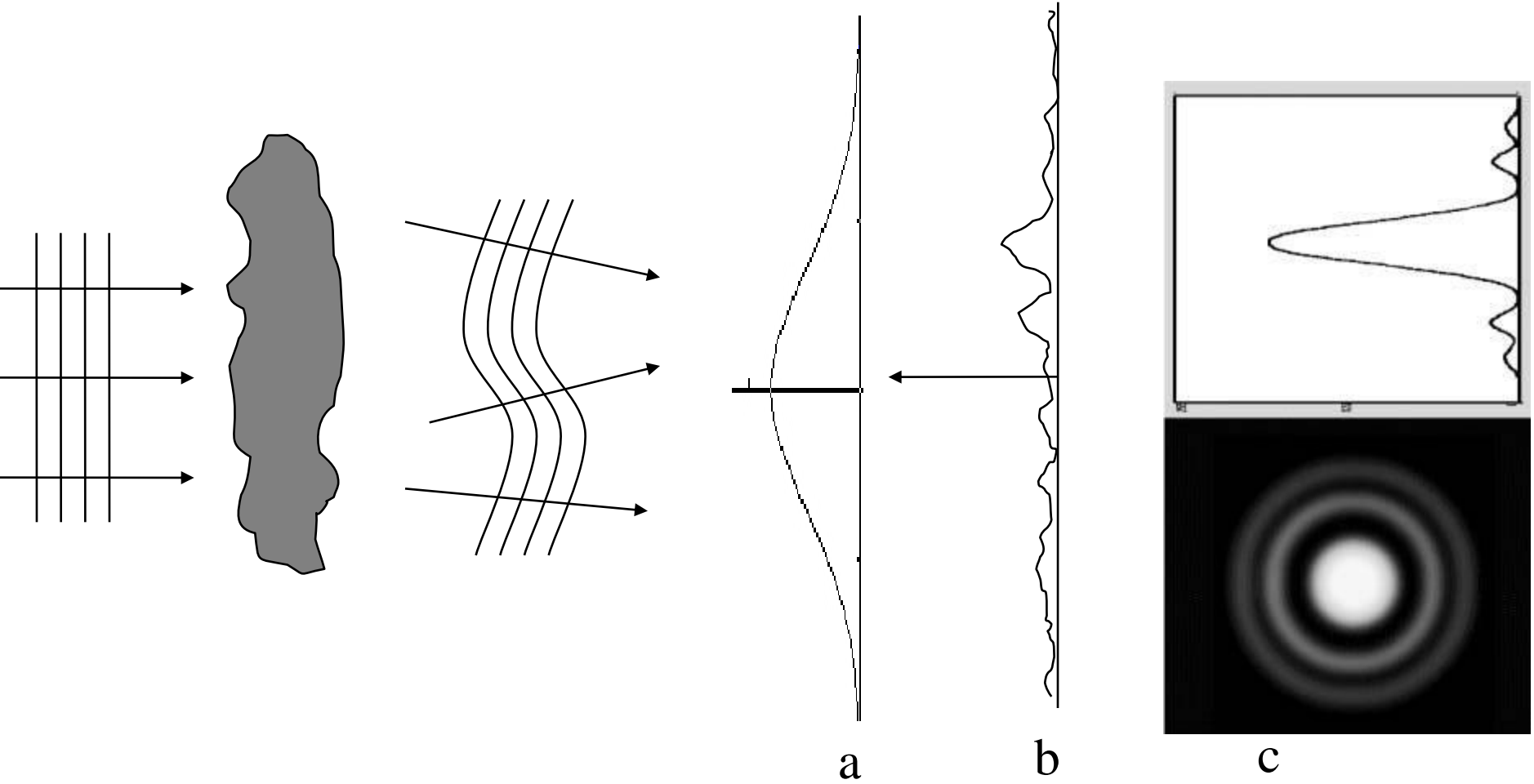
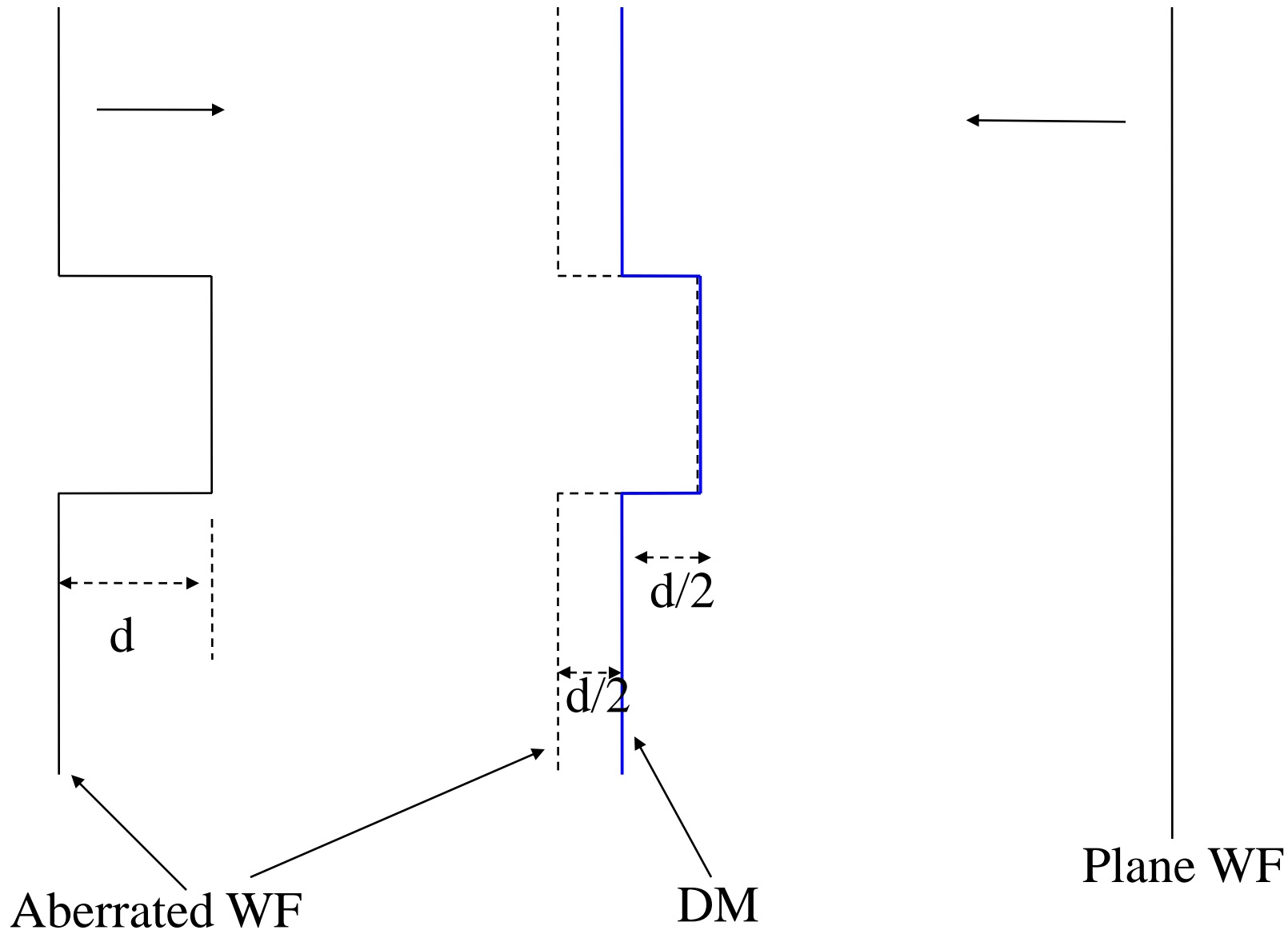


Adaptive Optics Reconstruction Methods

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Instrumentation Lab.
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Why do we need plane wavefront ?

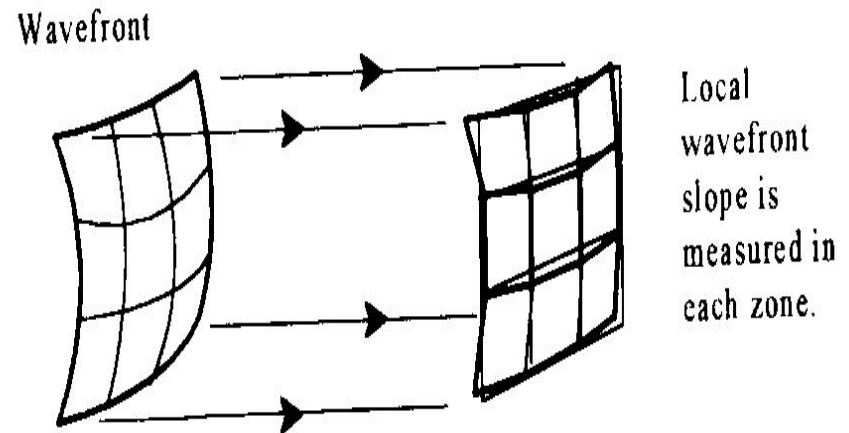




Wave Front Sensing

- Zonal wavefront sensing

Wavefront is expressed in terms of OPD over a small spatial area (zone/sub-aperture)

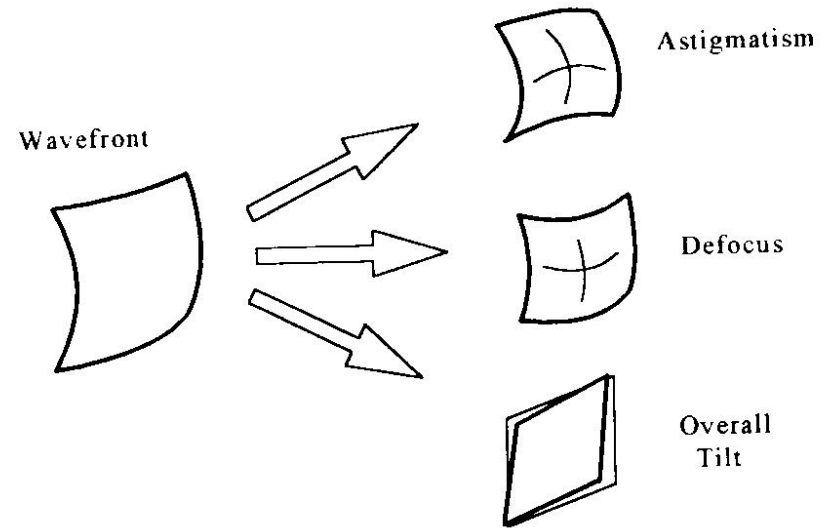


(a) Zonal wavefront sensing.

Wave Front Sensing

- **Modal Wavefront Sensing**

Wavefront is expressed in terms of some polynomial expansion over the entire pupil (i.e. PM)



(b) Modal wavefront sensing.

Zernike Polynomials

- WF can be expressed as Zernike polynomials
- Orthogonality of Zernike polynomials over unit circle
- Annular Zernike Polynomials

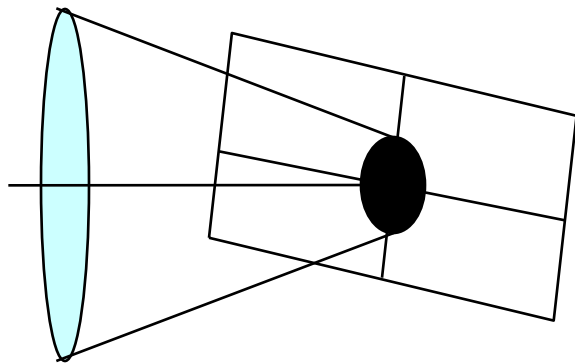
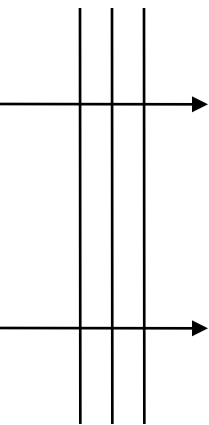
- Examples:

$z_1 = 1$	<i>piston</i>
$z_2 = 2r \cos \theta$	<i>x tilt</i>
$z_3 = 2r \sin \theta$	<i>y tilt</i>
$z_4 = \sqrt{3}(2r^2 - 1)$	<i>defocus</i>
$z_5 = \sqrt{6}r^2 \sin 2\theta$	<i>astigmatism</i>
$z_6 = \sqrt{6}r^2 \cos 2\theta$	<i>astigmatism</i>

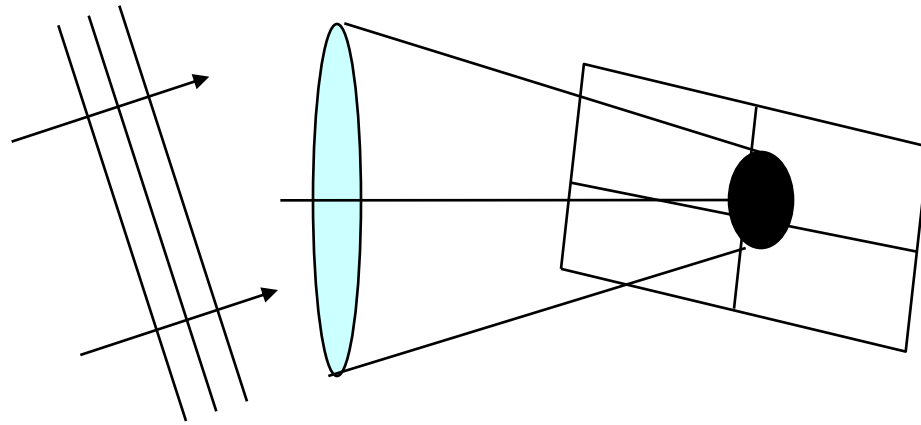
Zonal Wavefront Sensing

- Sub-aperture size & Fried parameter:
Refractive Index does not change over this region for the time interval of the order of , for example, 10 ms.
- Local tilts are measured.
- Centroid of intensity distribution is equal to shifted origin of the image plane; shift being proportional to the tilt (fig. (c) in next slide) , i.e. local tilt shifts centroid.

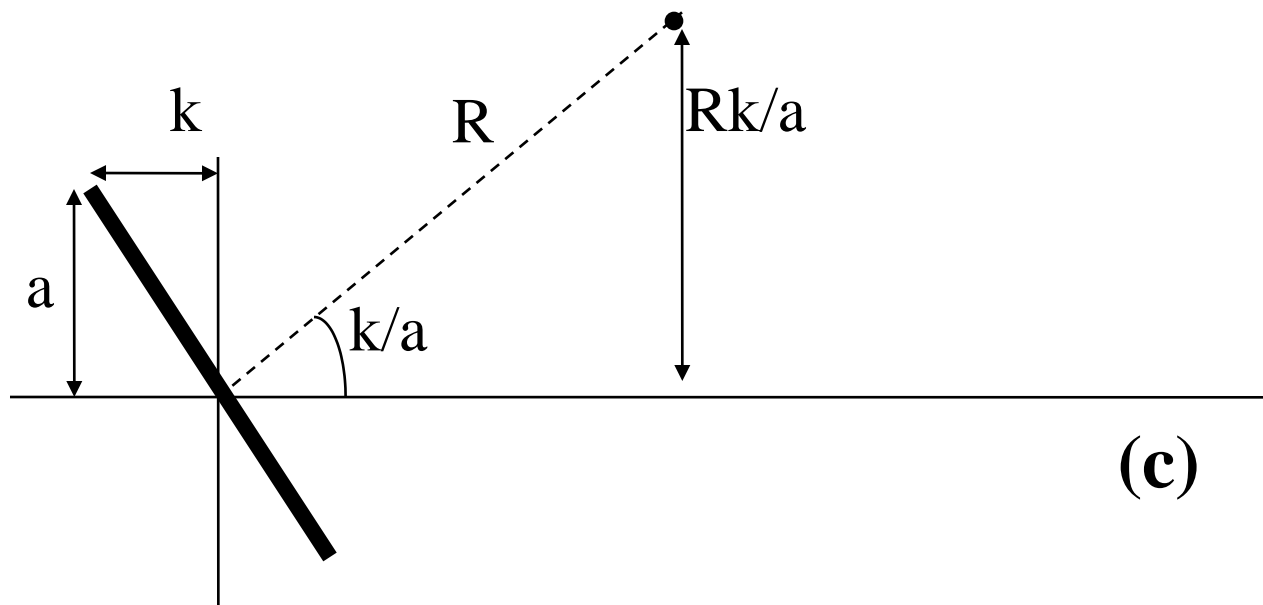
Zonal sensing



(a)

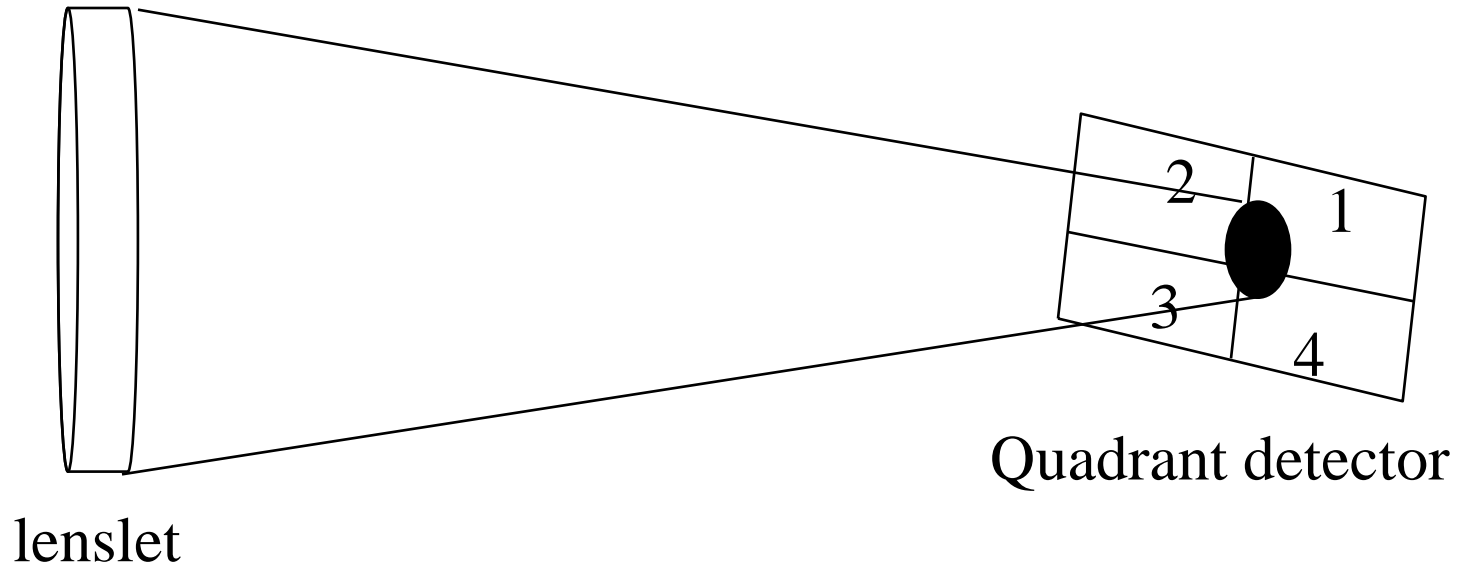


(b)



(c)

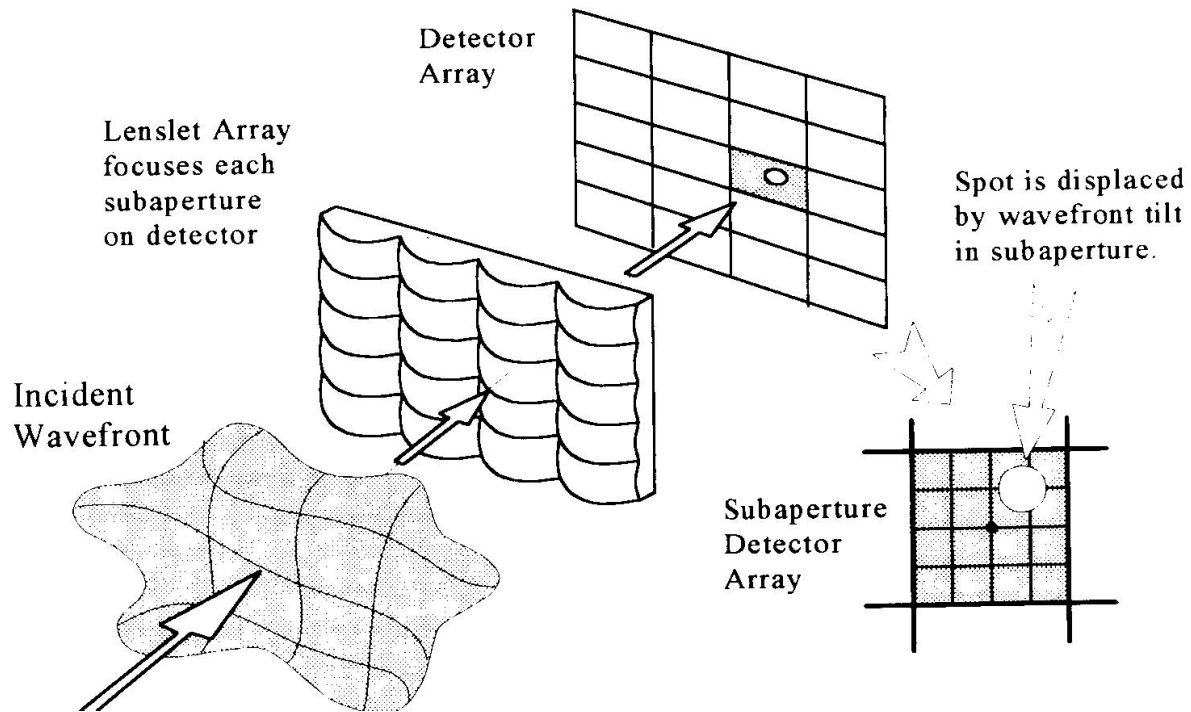
Zonal sensing



$$x_{centroid} = \frac{\int_1 Ids + \int_4 Ids - \int_2 Ids - \int_3 Ids}{\sum_i \int_i Ids}$$

$$y_{centroid} = \frac{\int_1 Ids + \int_2 Ids - \int_4 Ids - \int_3 Ids}{\sum_i \int_i Ids}$$

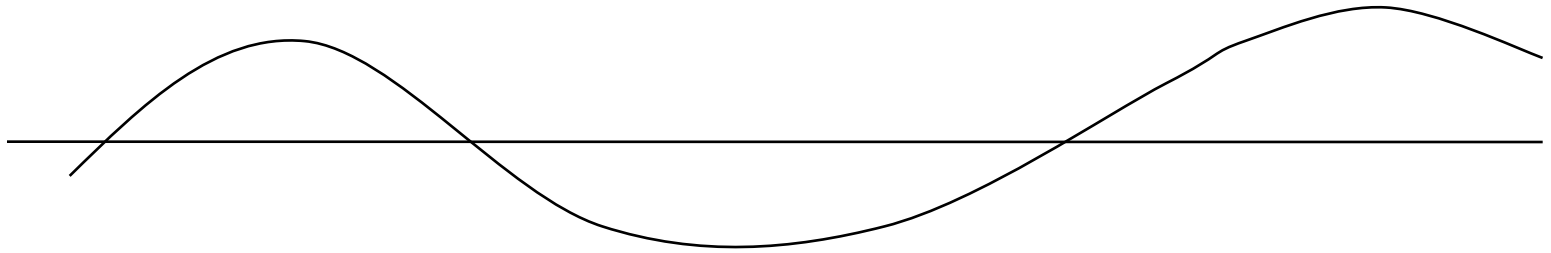
Shack-Hartmann Sensor



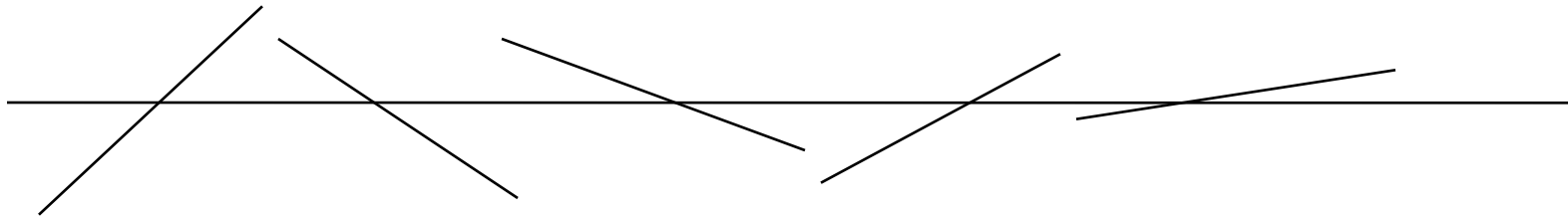
$$s(x, y) = \alpha(x, y) \cdot z$$

WF surface from slope measurements

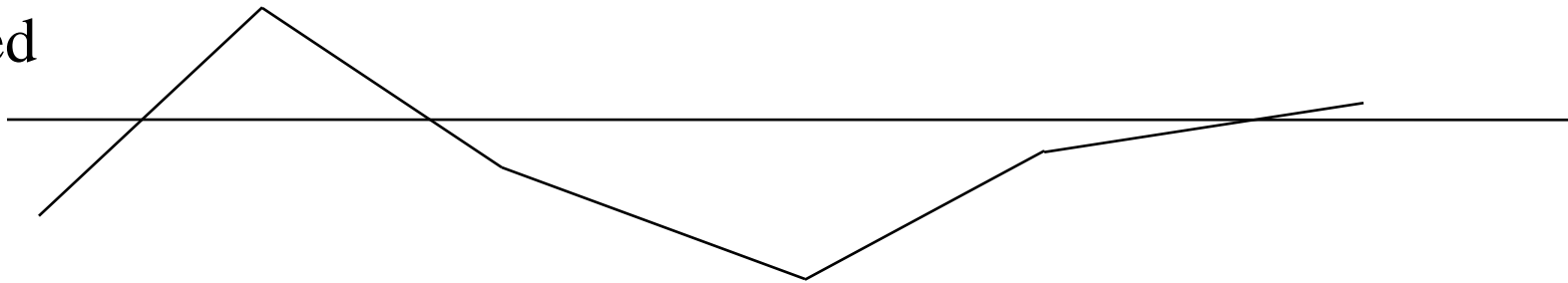
Original WF



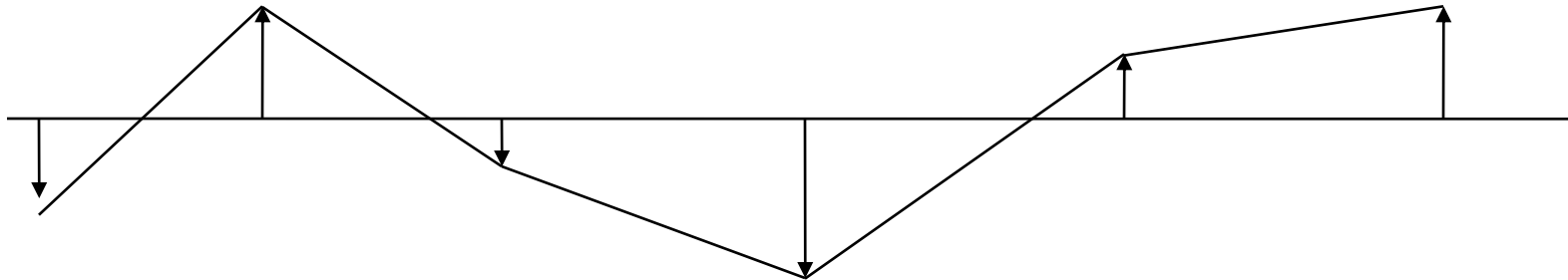
Zonal slopes
(one axis)



Reconstructed
WF



O/P to WF
corrector



Wavefront Reconstruction

(Phase/OPD from WF slopes)

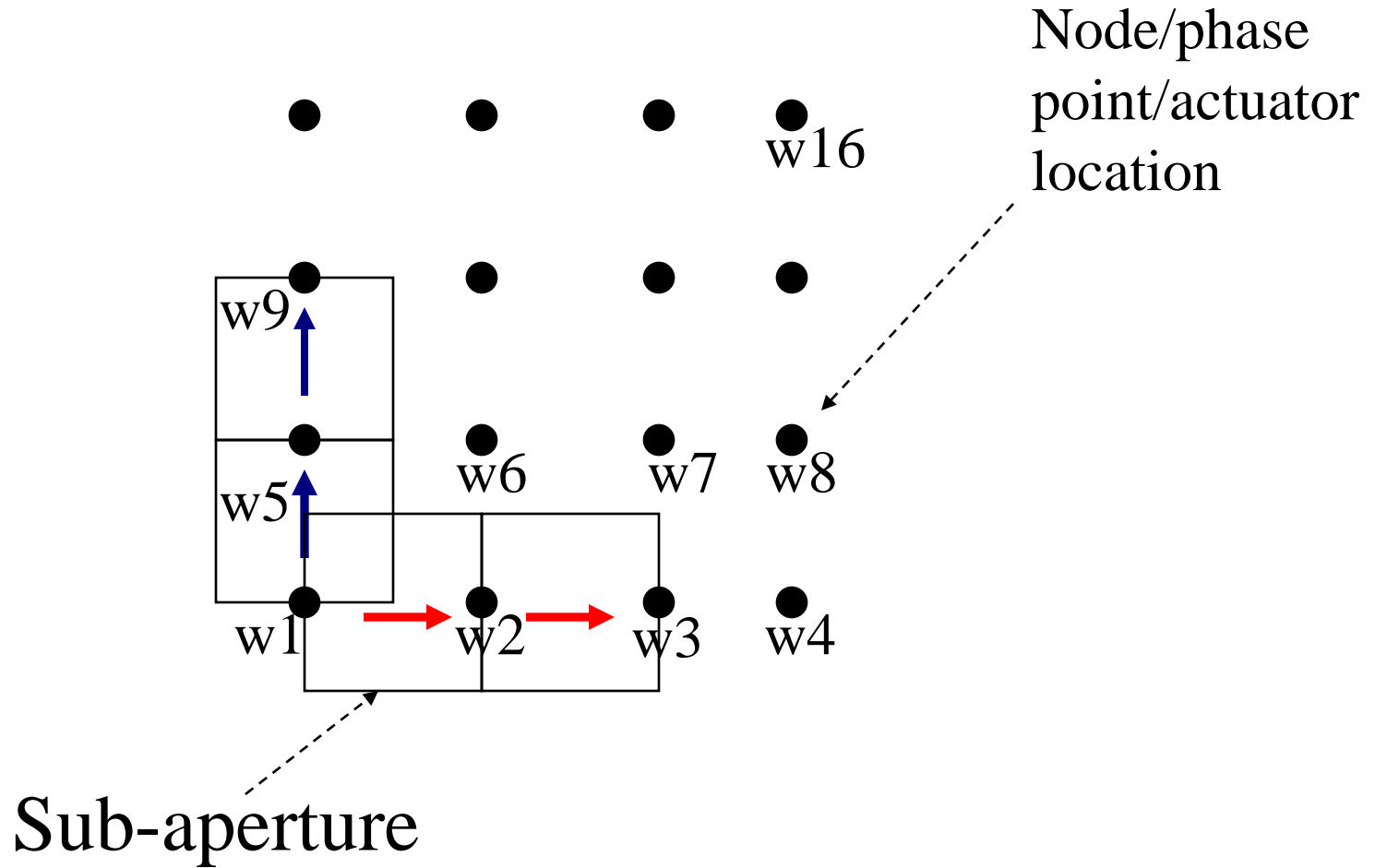
- OPD at **various points** on WF is determined from WF slopes at **other points** on the WF
- Number of WF slope measurements (M) is generally $>$ Number of unknown phase points (N)
- Problem of phase determination from WF slopes depends on geometry of arrangement of actuators w.r.t. phase points on WF

Wavefront Reconstruction

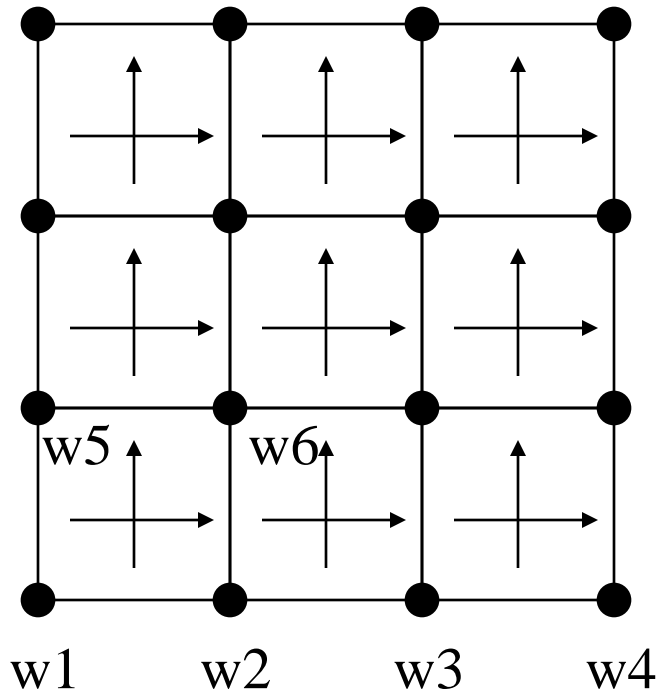
Main 3 Geometries :

- Hudgin
- Fried
- Southwell

Hudgin Geometry



Fried Geometry



Slope Model

$$\left(\frac{w_2 + w_6}{2} \right) - \left(\frac{w_1 + w_5}{2} \right) = s^x$$

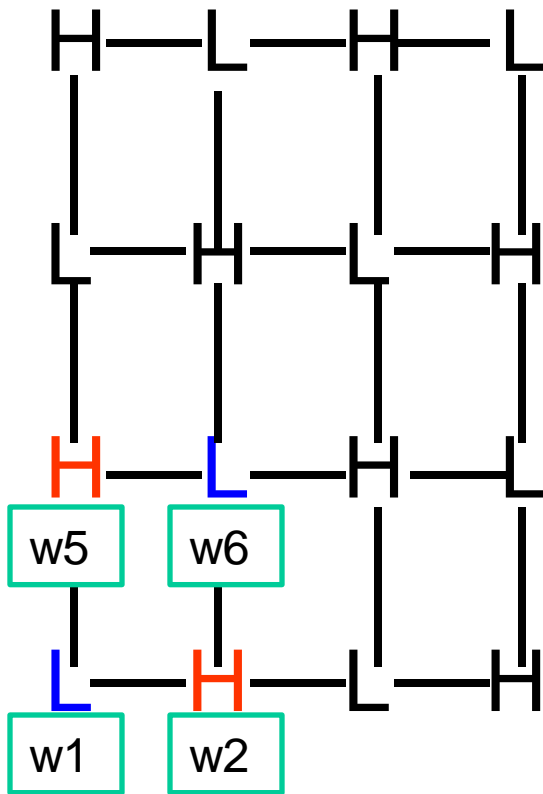
$$\left(\frac{w_5 + w_6}{2} \right) - \left(\frac{w_1 + w_2}{2} \right) = s^y$$

Waffle Mode (Fried geometry)

Two actuators on one diagonal are equally high and two actuators on the other diagonal are equally low.

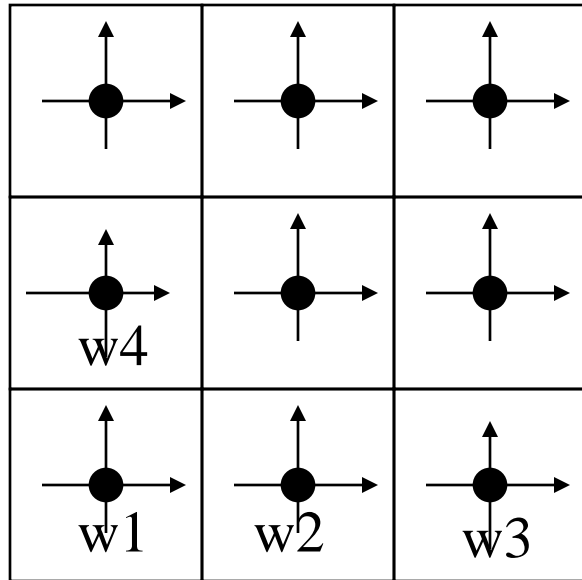
Centroid is undisturbed relative to centroid of flat wavefront.

Removal of waffle mode:



$$\frac{w_2 + w_5}{2} - \frac{w_1 + w_6}{2} = 0$$

Southwell Geometry



Slope Model

$$\frac{s_1^x + s_2^x}{2} = w_2 - w_1$$

$$\frac{s_1^y + s_4^y}{2} = w_4 - w_1$$

Slope Model (Hudgin Geometry)

$$w_2 - w_1 = s_1^x$$

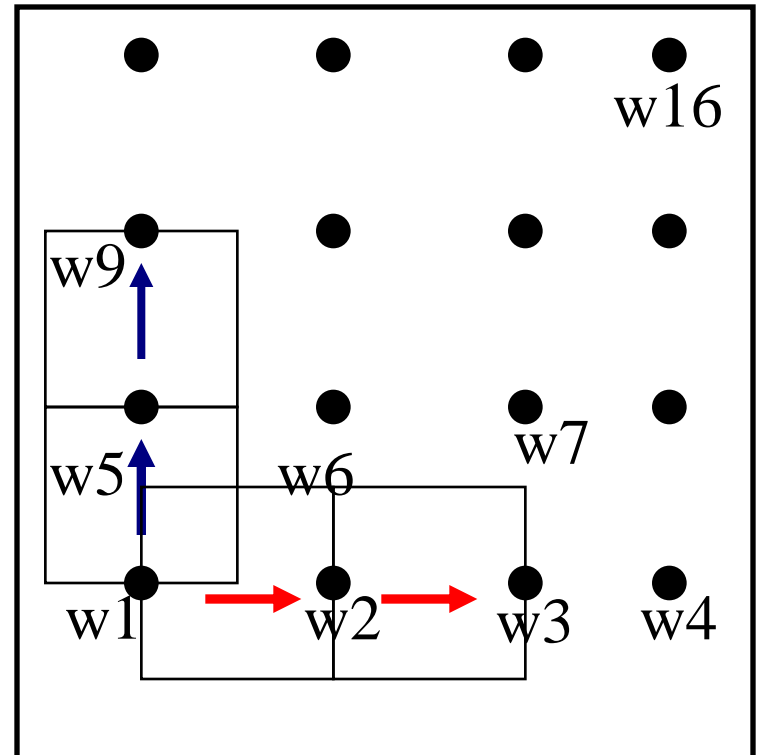
$$w_5 - w_1 = s_1^y$$

$$w_3 - w_2 = s_2^x$$

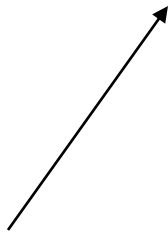
$$w_6 - w_2 = s_2^y$$

•
•
•

•
•
•



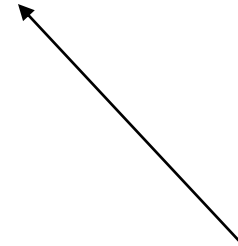
$$S_{M \times 1} = A_{M \times N} \cdot W_{N \times 1}$$



Slope measurements
from SH sensor



From geometry



To be estimated

Least Squares Method

$$\rightarrow [A] \cdot [W] = [S]$$

$$\rightarrow \text{Residual vector } [r] = [A] \cdot [W] - [S]$$

$$\rightarrow \|r\| = \|A\bar{W} - S\| \leq \|AW - S\| \text{ for all } W$$

$$\rightarrow \bar{W} = (A^T A)^{-1} A^T S$$

Difficulty: Every time $A^T A$ cannot be inverted.

Least squares method

$$\chi^2 = \sum_{i=1}^M \left[S_i - \sum_{k=1}^N A_{ik} \cdot W_k \right]^2$$

$$\frac{\partial}{\partial w_i} (\chi^2) = 0$$

$$W = [A^T A]^{-1} \cdot [A^T] \cdot S$$

Use of SVD

- Every MxN matrix can be factorized into 3 matrices

$$[A] = [U][D][V^T]$$

where

$$[D] = \begin{bmatrix} d_1 & & & & \\ & d_2 & & & \\ & & \cdot & & \\ & & & \cdot & \\ & & & & d_n \end{bmatrix}$$

$$[A^+] = [V][D^{-1}][U^T]$$

Pseudo-inverse:

$$[A^+] = [V] \begin{bmatrix} \frac{1}{d_1} & & & & \\ & \frac{1}{d_2} & & & \\ & & \cdot & & \\ & & & \cdot & \\ & & & & \frac{1}{d_N} \end{bmatrix} [U^T]$$

$$[D^{-1}] = \begin{cases} \frac{1}{d_i} & \text{if } d_i > t \\ 0 & \text{otherwise} \end{cases}$$

where t is a small threshold.

Finally we get the solution as:

$$\begin{aligned} [\bar{W}] &= [A^+][S] \\ &= [V][D^{-1}][U^T][S] \end{aligned}$$

References

- Adaptive Optics for Astronomical Telescopes; John W. Hardy; OUP 1998
- Linear Algebra; Gilbert Strang; Thomson/Brooks, Cole
- Wave-front Reconstruction from wave-front slope measurements; W.H. Southwell; J.Opt.Soc.Am., Vol.70, August 1980